

Tricam Geometry



Design and Operation

seepex Tricam Geometry is the natural evolution of the already proven 6L geometry. The unique characteristic of this new design is the double helix screw of the rotor in an elliptical cross section and the stator with a triple inter-

nal helix that has a pitch length, 50% longer than that of the rotor.

With this design, a third cavity is created that progresses through the pump with each rotation.

The Rotor and Stator

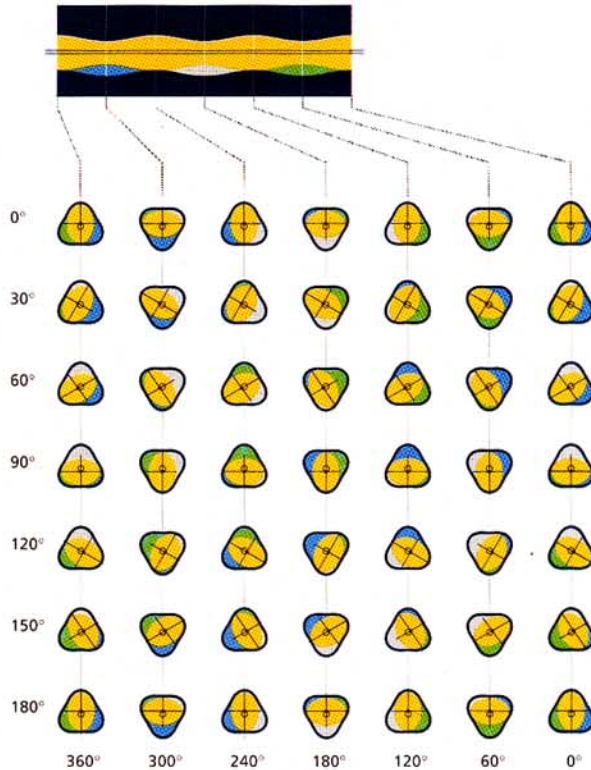
The Tricam rotor is of a double helix design that appears as an ellipsis in its cross section. The rotor maintains a circular eccentric motion as it rotates. The Tricam stator has a triple internal helix, each 120° opposed. Since the fluid cross section is unchanged during the pumping cycle, the Tricam design also delivers smooth, non-interrupted, predictable flow.

The Function

The rotor and stator combination creates three sealed cavities within the pump. The sealing lines defining these cavities are continuous, but revolve relative to each other, in their cross section. When the rotor revolves, the sealed cavities progress in a helical motion through the pump, displacing the captured liquids. Since these cavities are completely sealed, positively isolating the suction and discharge conditions from each other, the pump is capable of high suction lifts and high pressures, independent of its operating speed.

Interchangability

Due to the dimensional similarity of the 6L and Tricam elements, certain sizes of 6L pumps can be retrofitted with the Tricam design. If driver sizing allows, the Tricam exchange will deliver a 50% increase in the pump capacity. Conversely, the pump speed can be reduced by 1/3 and the pump will still deliver the original flow.

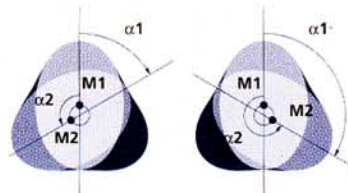


Increases Capacity by 50%

The ratio, $\alpha_2/\alpha_1 = 2$, is the basic operational feature that allows the Tricam design to dramatically increase capacity within a confined physical geometry, compared to the 1/2 screw design. Because the eccentric turning angle is twice the rotor turning angle, each of the three Tricam cavities progresses through the

pumping elements twice within each rotor revolution. The combined cross sectional fluid area of the 2/3 screw design is only approx. 75% of the area of the conventional design. Multiplying the 75% volume times the turning angle ratio of 2:1, provides an increase in total volume per revolution of 50%.

The Tricam Eccentric Track



Rotor Turning Angle
Eccentric Turning Angle

Position 1
 $\alpha_1 = 60^\circ$
 $\alpha_2 = 120^\circ$

Rotor Center Point
Rotor Center Point

$0^\circ = M1$
 $60^\circ = M2$

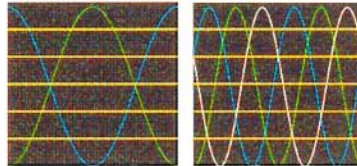
Position 2
 $\alpha_1 = 120^\circ$
 $\alpha_2 = 240^\circ$

$0^\circ = M1$
 $120^\circ = M2$

Tricam Advantages

- Compact Design** The **Tricam** design will increase flow by 50 % when compared with the 6L geometry of the same physical external dimensions.
- Reduced Surface Velocities and Reduced Axial Forces** Of special interest is the reduced surface velocity of the rotor, at the same capacity, and the slight reduction in axial load.
- Energy and Raw Materials Savings** The **Tricam** design saves users in two ways. Since smaller pumps can be used, less metal and elastomer is used to manufacture the **Tricam** design. The **Tricam** also has improved mechanical efficiencies. It takes less energy to manufacture and less energy to operate.

Improved Flow Properties

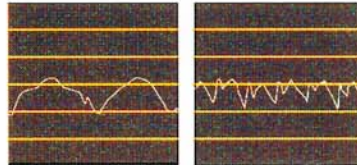


Capacity Curve – 6L

Capacity Curve – Tricam

Because the number of pumping chambers has been increased from two to three, fluid flow is more consistent.

Increased Pressure Stability



Static Pressure Diagram – 6L

Static Pressure Diagram – Tricam

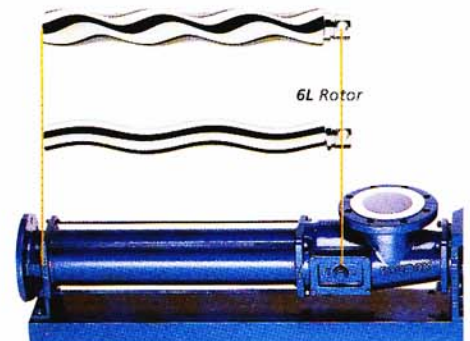
The higher pressure stability, specifically at lower operating speeds, makes the **Tricam** especially attractive for metering services.

The **Tricam** pumps have the same length and stator tube dimension as the previous design and can be readily interchanged into an existing pump.

Comparison of Technical Specification

| | 6L | Tricam |
|--|------------|---------------|
| Eccentric Speed $n(e)$ | $n(e) = n$ | $n(e) = 2n$ |
| Number of Chambers | 2 | 3 |
| Chamber Volume | 100 % | approx. 75 % |
| Capacity | 100 % | approx. 150 % |
| Power Requirement | 100 % | approx. 145 % |
| Particle Velocity ($n = \text{constant}$) | 100 % | 200 % |
| Particle Velocity ($Q = \text{constant}$) | 100 % | approx. 140 % |
| Thrust Load | 100 % | approx. 120 % |
| Maximum Solids Size | 100 % | approx. 68 % |
| Volumetric Efficiency | + | ++ |
| Overall Efficiency | + | ++ |
| Pulsations | + | ++ |
| Physical Size | + | ++ |
| Average Surface Velocity ($n = \text{constant}$) | 100 % | approx. 110 % |
| Average Surface Velocity ($Q = \text{constant}$) | 100 % | approx. 75 % |

Tricam Rotor



Tricam Dimensions

| Dimensions | 15-6LT | 30-6LT | 40-6LT | 55-6LT | 75-6LT | 110-6LT |
|------------|--------|--------|--------|--------|--------|---------|
| a | 68 | 73 | 80 | 80 | 80 | 90 |
| a1 | 41 | 43 | 52 | 43 | 43 | 45 |
| a2 | 733 | 912 | 1059 | 1088 | 1196 | 1370 |
| a3 | — | — | — | — | — | — |
| a4 | 205 | 230 | 260 | 265 | 265 | 310 |
| b | 95 | 105 | 110 | 120 | 120 | 145 |
| b1 | 115 | 125 | 125 | 150 | 150 | 150 |
| c | 12 | 14 | 15 | 15 | 15 | 15 |
| f | 120 | 140 | 145 | 155 | 155 | 185 |
| f1 | 140 | 155 | 160 | 180 | 180 | 200 |
| h | 100 | 125 | 130 | 140 | 140 | 160 |
| h1 | 210 | 245 | 260 | 285 | 290 | 320 |
| i | 86 | 102 | 110 | 120 | 120 | 141 |
| k | 875 | 1066 | 1235 | 1255 | 1363 | 1561 |
| k1 | 1065 | 1287 | 1481 | 1516 | 1624 | 1866 |
| m | 48 | 50 | 50 | 50 | 50 | 60 |
| m1 | 134 | 149 | 164 | 164 | 164 | 196 |
| n | 20 | 20 | 20 | 20 | 20 | 20 |
| n1 | 33 | 38 | 44 | 44 | 44 | 56 |
| o1 | 628 | 777 | 921 | 926 | 1034 | 1180 |
| p | 410 | 520 | 590 | 645 | 765 | 845 |
| q1 | G 1/4" | G 3/8" | G 3/8" | G 3/8" | G 3/8" | G 1/2" |
| q2 | G 1/2" | G 1/2" | G 1/2" | G 1/2" | G 3/4" | G 3/4" |
| s | 12 | 14 | 14 | 14 | 14 | 18 |

| Drive End | | | | | | |
|-----------|----|----|----|----|----|------|
| d | 25 | 30 | 35 | 40 | 40 | 50 |
| l | 50 | 65 | 70 | 75 | 75 | 90 |
| t | 28 | 33 | 38 | 43 | 43 | 53,5 |
| u | 8 | 8 | 10 | 12 | 12 | 14 |

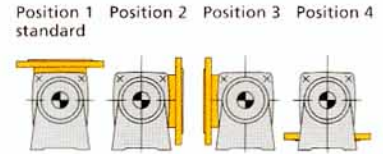
| Suction Connection ANSI B 16,5 ¹⁾ | | | | | | |
|--|------|------|------|------|------|------|
| DIN | 2501 | 2501 | 2501 | 2501 | 2501 | 2501 |
| PN | 16 | 16 | 16 | 16 | 16 | 16 |
| DN1 | 80 | 100 | 100 | 125 | 125 | 150 |
| D1 ²⁾ | 200 | 220 | 220 | 250 | 250 | 285 |
| K1 | 160 | 180 | 180 | 210 | 210 | 240 |
| S1 | 18 | 18 | 18 | 18 | 18 | 23 |
| Z1 | 8 | 8 | 8 | 8 | 8 | 8 |

| Discharge Connection ANSI 16,5 ¹⁾ | | | | | | |
|--|------|------|------|------|------|------|
| DIN | 2501 | 2501 | 2501 | 2501 | 2501 | 2501 |
| PN | 16 | 16 | 16 | 16 | 16 | 16 |
| DN2 | 65 | 80 | 100 | 100 | 125 | 125 |
| D2 ²⁾ | 185 | 200 | 220 | 220 | 250 | 250 |
| K2 | 145 | 160 | 180 | 180 | 210 | 210 |
| S2 | 18 | 18 | 18 | 18 | 18 | 18 |
| Z2 | 4 | 8 | 8 | 8 | 8 | 8 |

| Weight [lbs] approx. | | | | | | |
|----------------------|----|----|----|-----|-----|-----|
| BN | 37 | 57 | 85 | 104 | 119 | 152 |
| NS | 39 | 60 | 90 | 110 | 125 | 160 |

Suction Branch Position¹⁾

Range **BN** viewed from drive end
Range **NS** viewed from pump shaft



ANSI Pump Flanges

| Flange to DIN 2501 | Flange to ANSI B16,5 | 150 lbs | | |
|--------------------|----------------------|---------|-------|-------|
| DN | DN | K1 K2 | S1 S2 | Z1 Z2 |
| 65 | 2 1/2" | 139,7 | 19,1 | 4 |
| 80 | 3" | 152,4 | 19,1 | 4 |
| 100 | 4" | 190,5 | 19,1 | 8 |
| 125 | 5" | 215,9 | 22,4 | 8 |
| 150 | 6" | 241,3 | 22,4 | 8 |

- 1) For normal operation pump rotation is counterclockwise, suction connection = **DN1**, pressure connection = **DN2**. For reverse flow clockwise rotation the suction and discharge connections are reversed i.e. suction connection now **DN2**, pressure connection now **DN1**.
- 2) Minor deviations might occur with flange external diameters **D1** and **D2** since larger DIN flange diameters have been machined to ANSI specifications.

Range BN

Drive Choice:
Gearmotor
Variable Speed Drive
Hydraulic Motor

* Dimension for Stator Replacement
** Number of Holes

Range NS

* Dimension for Stator Replacement
** Number of Holes

Shaft Key acc. DIN 6885

Tricam Performance Data

Sizing

Due to the number of variables that must be considered for proper pump sizing; such as, fluid rheology, adhesive or cohesive reactions, suction conditions, viscosity, other physical fluid properties and temperature, all selections should be confirmed by seepex. The sizing of the required driver can be approximated from the table below, regard should be given to the safety factors particularly to the efficiency and torque characteristics of the preferred drive.

The data in the table below is the minimum requirement at the pump shaft. For drive sizing, starting power must be calculated with the following formula:

$$P_A \text{ [kW]} = \frac{M_A \text{ [Nm]}^{*1} \times n \text{ [min}^{-1}\text{]}}{9550 \times M_A / M_A^{*2}}$$

Drive

For the selection of the proper drive, it is necessary to use the higher of the required operating power or the required starting power. Drive efficiency must always be considered. The consideration of starting power requirements is critical due to the compression fit between the rotor and stator in seepex pumps. seepex strives to maintain an optimum compression to minimize starting power but to maximize volumetric efficiencies, suction lift capabilities, pressure stability and pumping element life.

A pump with compression fit between the pumping elements offers the following advantages over pumps with clearance fits between the pumping elements:

- ~ Minimal internal slippage which results in less wear on the pumping elements.
- ~ Improved volumetric efficiencies over a wide speed range at a given differential pressure.
- ~ High suction lift capability (low NPSHr) even at low speeds.

*1
The starting torque value is dependent on the product being pumped. Lubricating type materials with low viscosities will require less starting torque then will adhesive, solids laden or viscous materials.

*2
The starting power factor depends on the type of drive selected. Consult the data listed in the drive manufacturer's published literature.

| Q [m³/h] | bar | 15-6LT M _A 70 – 100 Nm | | | 30-6LT M _A 105 – 150 Nm | | | 40-6LT M _A 140 – 200 Nm | | | 55-6LT M _A 175 – 250 Nm | | | 75-6LT M _A 245 – 350 Nm | | | 110-6LT M _A 315 – 450 Nm | | |
|----------|-----------|--------------------------------------|-------------|-------------|---------------------------------------|-------------|-------------|---------------------------------------|-------------|-------------|---------------------------------------|-------------|-------------|---------------------------------------|-------------|-------------|--|-------------|-------------|
| | | 2 | 4 | 6 | 2 | 4 | 6 | 2 | 4 | 6 | 2 | 4 | 6 | 2 | 4 | 6 | 2 | 4 | 6 |
| 2 | upm kW | 54 0,35 | 64 0,54 | 82 0,86 | | | | | | | | | | | | | | | |
| 3 | upm kW | 78 0,51 | 88 0,76 | 106 1,11 | | | | | | | | | | | | | | | |
| 4 | upm kW | 102 0,66 | 112 0,95 | 130 1,36 | | | | | | | | | | | | | | | |
| 5 | upm kW | 126 0,82 | 136 1,16 | 154 1,62 | 58 0,65 | 75 1,19 | 91 1,89 | | | | | | | | | | | | |
| 7,5 | upm kW | 187 1,21 | 197 1,67 | 215 2,25 | 86 0,97 | 103 1,65 | 119 2,48 | 65 0,97 | 81 1,73 | 96 2,69 | | | | | | | | | |
| 10 | upm kW | 247 1,61 | 257 2,19 | 275 2,89 | 114 1,29 | 131 2,10 | 148 3,06 | 86 1,28 | 102 2,17 | 119 3,27 | 64 1,28 | 80 2,30 | 97 3,61 | | | | | | |
| 12,5 | upm kW | 308 2,00 | 318 2,70 | 335 3,52 | 143 1,60 | 159 2,55 | 176 3,65 | 107 1,60 | 123 2,62 | 140 3,85 | 79 1,59 | 96 2,74 | 113 4,19 | 54 1,63 | 71 3,20 | 88 5,26 | | | |
| 15 | upm kW | 368 2,39 | 378 3,21 | 396 4,16 | 171 1,92 | 187 3,00 | 204 4,23 | 128 1,91 | 144 3,07 | 161 4,42 | 95 1,90 | 112 3,19 | 128 4,76 | 65 1,95 | 82 3,67 | 98 5,89 | 54 2,05 | 62 3,45 | 78 5,75 |
| 17,5 | upm kW | 428 2,78 | 438 3,73 | 456 4,79 | 199 2,24 | 216 3,45 | 232 4,82 | 149 2,23 | 165 3,51 | 182 5,00 | 111 2,21 | 127 3,63 | 144 5,34 | 76 2,27 | 92 4,15 | 109 6,53 | 62 2,34 | 69 3,87 | 85 6,31 |
| 20 | upm kW | | | | 227 2,56 | 244 3,90 | 260 5,40 | 170 2,54 | 186 3,96 | 203 5,58 | 126 2,52 | 143 4,08 | 159 5,92 | 86 2,58 | 103 4,62 | 119 7,16 | 69 2,63 | 77 4,29 | 93 6,87 |
| 25 | upm kW | | | | 284 3,19 | 300 4,80 | 317 6,58 | 212 3,17 | 228 4,85 | 245 6,73 | 157 3,15 | 174 4,97 | 191 7,08 | 107 3,22 | 124 5,57 | 140 8,43 | 84 3,20 | 92 5,14 | 108 7,99 |
| 30 | upm kW | | | | 340 3,83 | 357 5,71 | 373 7,75 | 254 3,80 | 270 6,74 | 287 7,89 | 188 3,77 | 205 5,86 | 222 8,23 | 128 3,85 | 145 6,52 | 162 9,69 | 99 3,78 | 107 5,99 | 123 9,11 |
| 40 | upm kW | | | | 396 4,46 | 413 6,61 | 430 8,92 | 338 5,06 | 354 7,53 | 371 10,2 | 251 5,01 | 267 7,64 | 284 10,6 | 171 5,12 | 187 8,42 | 204 12,2 | 130 4,93 | 137 7,68 | 153 11,4 |
| 50 | upm kW | | | | | | | 422 6,33 | 438 9,31 | 455 12,5 | 313 6,26 | 330 9,42 | 346 12,9 | 213 6,39 | 229 10,3 | 246 14,8 | 160 6,08 | 167 9,38 | 184 13,6 |
| 60 | upm kW | | | | | | | | | | 375 7,50 | 392 11,2 | 408 15,2 | 255 7,65 | 272 12,2 | 288 17,3 | 190 7,23 | 198 11,1 | 214 15,8 |
| 70 | upm kW | | | | | | | | | | | | | 297 8,92 | 314 14,1 | 331 19,8 | 221 8,38 | 228 12,8 | 244 18,1 |
| 80 | upm kW | | | | | | | | | | | | | | | | 251 9,53 | 258 14,5 | 274 20,3 |

All performance data is approximated, based on H₂O @ 20° C, subject to change without notice.

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